

MEP451

Cooling Load Calculation

RTS

Radiant Time Series Method

Aug. 2009

1

Steps for performing the RTS method

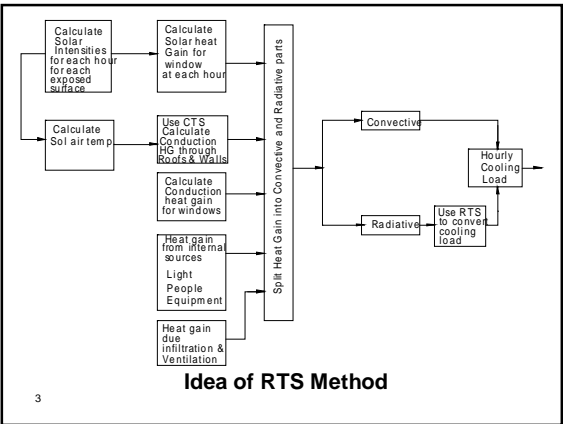
1- Calculate the heat gain due to all sources
[Externally and internally]

2-Split the heat gains into convective and radiative part
according to the type of the heat gain

3-Treat the radiative heat gain using RTS to
convert it to cooling load

4-Sum the convective heat gain plus the cooling load due
to the radiative heat gain to get the total cooling load

2



Converting Radiative heat gain into cooling load

Radiant time factor

$$Q_{CL,r,q} = \sum_{n=0}^{n=23} r_n Q_{HG,r,q-n\Delta t} = r_0 Q_{HG,r,q} + r_1 Q_{HG,r,q-1} + r_2 Q_{HG,r,q-2} + \dots$$

Cooling Load
At time θ

Radiative Heat Gains

4

Hourly outdoor temperature & Sol-air temperature

$$t_o = t_d - DR * (X)$$

Long wave radiation correction

$$t_e(hr) = t_o(hr) + \alpha G_t / h_o - \epsilon dR / h_o$$

0 for vertical surface

7° F (3.9°C) for horizontal surface

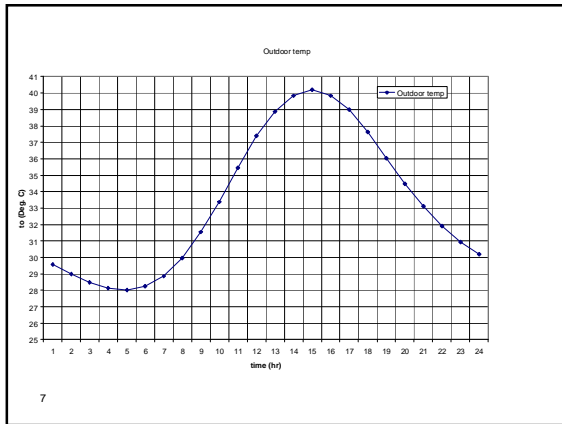
$\alpha(\text{Around}) = 0.9,$
 $h_o = 34 \text{ W/m}^2 \cdot \text{K}$

5

Example 12.1 Hourly outdoor temperature
td=40.2° C, DR=12.2° C [Jeddah 0.4 % design]

Solar time	Outdoor Temp. t_o	Solar time	Outdoor Temp. t_o	Solar time	Outdoor Temp. t_o	Solar time	Outdoor Temp. t_o
1	29.6	7	28.9	13	38.9	19	36.1
2	29.0	8	30.0	14	39.8	20	34.5
3	28.5	9	31.5	15	40.2	21	33.1
4	28.1	10	33.4	16	39.8	22	31.9
5	28.0	11	35.4	17	39.0	23	30.9
6	28.2	12	37.4	18	37.6	24	30.2

6



Heat Gains

- ØConduction through exposed walls and roofs
- ØConduction through un-exposed (Partitions) walls
- ØWindows
- ØLights
- ØPeople
- ØEquipment
- ØInfiltration & Ventilation

8

Conduction Heat Gain due to sunlit walls and roofs

Conduction Heat Gain

$$Q_{HG,q} = \sum_{n=0}^{n=23} c_n Q_{i,q-nd} = c_0 Q_{i,q} + c_1 Q_{i,q-1} + c_2 Q_{i,q-2} + \dots$$

Heat input

$$Q_{i,q} = UA(t_{e,q} - t_r)$$

Conduction Time series CTS

9

CTS for Walls

Time (hr)	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24
Q _{i,q}	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
Q _{i,q-1}	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Q _{i,q-2}	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

10

CTS for Walls (continue)

Time (hr)	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24
Q _{i,q}	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
Q _{i,q-1}	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Q _{i,q-2}	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

11

CTS for Roofs

Time (hr)	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24
Q _{i,q}	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
Q _{i,q-1}	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Q _{i,q-2}	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

12

New ASHRAE layer Definition

Layer	Material	Thickness (mm)	Thermal Conductivity (W/mK)	Thermal Capacity (J/m²K)	Thermal Resistance (m²K/W)	Thermal Mass (J/m²K)
1	Concrete	100	1.4	1000	0.071	100000
2	Concrete	100	1.4	1000	0.071	100000
3	Concrete	100	1.4	1000	0.071	100000
4	Concrete	100	1.4	1000	0.071	100000
5	Concrete	100	1.4	1000	0.071	100000
6	Concrete	100	1.4	1000	0.071	100000
7	Concrete	100	1.4	1000	0.071	100000
8	Concrete	100	1.4	1000	0.071	100000
9	Concrete	100	1.4	1000	0.071	100000
10	Concrete	100	1.4	1000	0.071	100000
11	Concrete	100	1.4	1000	0.071	100000
12	Concrete	100	1.4	1000	0.071	100000
13	Concrete	100	1.4	1000	0.071	100000
14	Concrete	100	1.4	1000	0.071	100000
15	Concrete	100	1.4	1000	0.071	100000
16	Concrete	100	1.4	1000	0.071	100000
17	Concrete	100	1.4	1000	0.071	100000
18	Concrete	100	1.4	1000	0.071	100000
19	Concrete	100	1.4	1000	0.071	100000
20	Concrete	100	1.4	1000	0.071	100000
21	Concrete	100	1.4	1000	0.071	100000
22	Concrete	100	1.4	1000	0.071	100000
23	Concrete	100	1.4	1000	0.071	100000
24	Concrete	100	1.4	1000	0.071	100000

Example 12.3 Given t_e , G , Wall #21, Find Heat input and heat gain

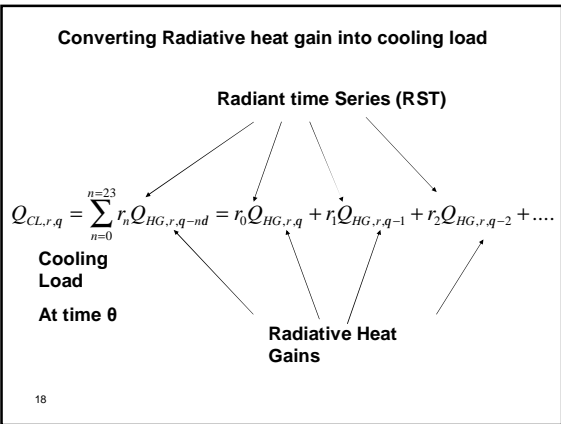
hr	G_t	hr	G_t
1	0	13	377.8
2	0	14	484.2
3	0	15	534.6
4	0	16	513.6
5	0	17	399.2
6	22	18	126.7
7	81.5	19	0
8	125	20	0
9	158.8	21	0
10	183.7	22	0
11	203.4	23	0
12	230.4	24	0

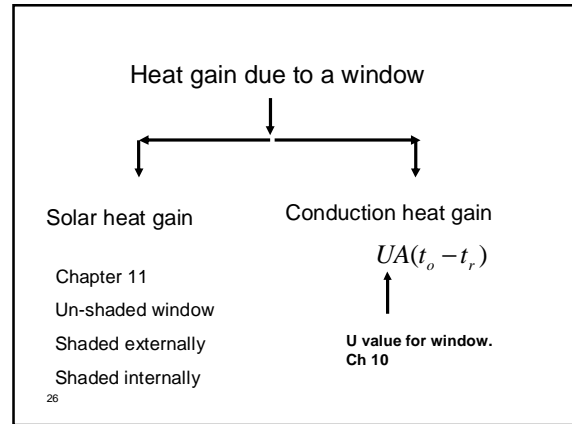
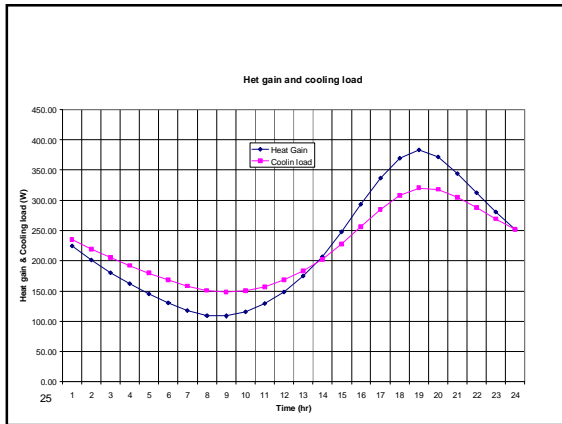
Ts [hr]	t_e	G_t	t_e	CTS	Heat input [W/m²]	Heat gain[W/m²]
1	29.4	0	29.4	0	2.06	5.00
2	28.8	0	28.8	0.04	1.83	4.46
3	28.3	0	28.3	0.13	1.64	4.01
4	27.9	0	27.9	0.16	1.50	3.60
5	27.8	0	27.8	0.14	1.46	3.23
6	28.0	22	28.6	0.11	1.77	2.89
7	28.7	81.5	30.8	0.09	2.61	2.62
8	29.8	125	33.1	0.07	3.47	2.43
9	31.3	158.8	35.5	0.06	4.42	2.41
10	33.2	183.7	38.0	0.04	5.37	2.57
11	35.2	203.4	40.6	0.03	6.37	2.87
12	37.2	230.4	29.4	0.03	7.39	3.31
13	38.7	377.8	48.7	0.02	9.44	3.88
14	39.6	484.2	52.5	0.02	10.90	4.60
15	40.0	534.6	54.2	0.02	11.55	5.51
16	39.6	513.6	53.2	0.01	11.19	6.53
17	38.8	399.2	49.3	0.01	9.71	7.49
18	37.4	126.7	40.8	0.01	6.43	8.22
19	35.9	0	35.9	0.01	4.54	8.51
20	34.3	0	34.3	0	3.93	8.26
21	32.9	0	32.9	0	3.42	7.66
22	31.7	0	31.7	0	2.95	6.94
23	30.7	0	30.7	0	2.58	6.24
24	30.0	0	30.0	0	2.30	5.50

Converting Radiative Heat Gain into Cooling Load

Zone Types

Zone Type	Envelope	Roof/Floor	Walls	Partitions	Floor	Roof/Floor
Office	100 mm concrete	100 mm concrete	100 mm concrete	100 mm concrete	100 mm concrete	100 mm concrete
Residential	100 mm concrete	100 mm concrete	100 mm concrete	100 mm concrete	100 mm concrete	100 mm concrete
Hotel	100 mm concrete	100 mm concrete	100 mm concrete	100 mm concrete	100 mm concrete	100 mm concrete





Calculation of heat gains

Conduction Heat gain through windows including the frame

$$Q = (U_g A_g + U_f A_f)(t_o - t_r)$$

Window U value, Table 10.6
Frame U, Table 10.8

Split conduction heat gain into convective and radiative parts

27

Calculation of heat gains

Solar Heat Gain due to a window

$$\dot{Q}_{SHG} = [SHGC_{g,b} A_{gl,g} + SHGC_f A_{gl,f}] G_D + [SHGC_{gd} A_g + SHGC_f A_f] G_d$$

Table 11.3
 $SHGC_f = a_f \left[\frac{U_f A_f}{h_o A_{surf}} \right]$

28

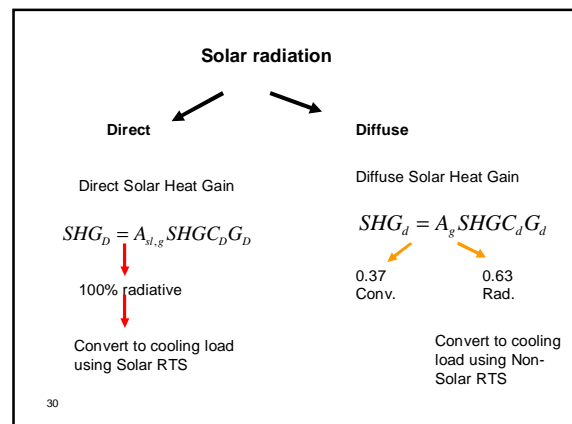
Calculation of heat gains

Solar Heat Gain for internally shaded window

$$\dot{Q}_{SHG} = [SHGC_f A_{gl,f} G_D + SHGC_f A_f G_d] + [SHGC_{gd} A_{gl,g} G_D + SHGC_{gd} A_g G_d] IAC$$

IAC=Interior Attenuation Coefficient

29



Case with indoor shade

• Add all heat gains i.e. direct diffuse and conduction heat.

• Separate heat gain into conductive and radiative

• Treat the radiative HG using non solar RTS

31

Calculation of heat gains

Heat gain due to lights

a) When the total wattage, use factor, and special allowance factor are given

$$Q = W * F_u * F_s \quad [W]$$

W = Total wattage

F_u Use factor=% of lights that are in operation

F_s=Special allowance factor. F_s=1. for tungsten lights, F_s=1.2 for Fluorescent lights

32

Calculation of heat gains

Heat gain due to lights

b) When the density (Watt per unit area) of lights is known

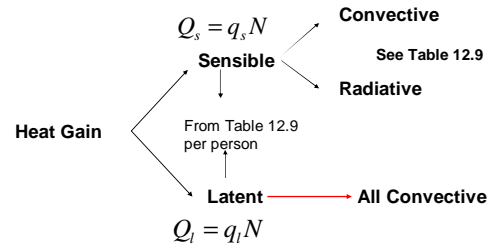
$$Q = \text{Flux density} * A$$

A= Plan area

33

Calculation of heat gains

Heat gain due people



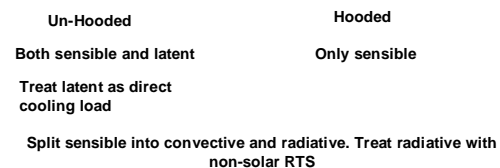
34

Table 12.9 Heat gain due to people

Type of activity	Typical clothing	Total Heat Gain		Sensible Heat Gain, W	Latent Heat Gain, W	% Sensible Heat Gain of Total	
		Adult Male	Adult Female				
Light work	Typical clothing	115	95	45	70	39	37
Medium work	Typical clothing	135	115	55	80	41	39
Heavy work	Typical clothing	155	135	65	90	42	39
Very heavy work	Typical clothing	175	155	75	100	43	39
Light work	Typical clothing	115	95	45	70	39	37
Medium work	Typical clothing	135	115	55	80	41	39
Heavy work	Typical clothing	155	135	65	90	42	39
Very heavy work	Typical clothing	175	155	75	100	43	39
Light work	Typical clothing	115	95	45	70	39	37
Medium work	Typical clothing	135	115	55	80	41	39
Heavy work	Typical clothing	155	135	65	90	42	39
Very heavy work	Typical clothing	175	155	75	100	43	39

35

Heat gain due equipment in space



36

See Appendix B for typical of values of heat gains from equipment

Calculation of heat gains

Cooling Load due to Infiltration

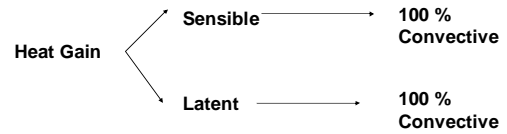
Heat Gain $\dot{Q}_i = \dot{m}_a (h_o - h_r)$

\dot{m}_a Mass flow rate of infiltration air

37

Calculation of heat gains

Cooling Load due to Infiltration



38

Calculation of heat gains

Cooling Load due to Infiltration

Heat Gain [W]

Sensible

$$\dot{Q}_s = \dot{m}_a C_p (t_o - t_i)$$

$$\dot{Q}_s = \frac{\dot{V}}{v} * 1.0 * (t_o - t_i)$$

$$\dot{Q}_s = 1.2 * \dot{V} * (t_o - t_i)$$

Latent

$$\dot{Q}_l = \dot{m}_a (W_o - W_i) h_{fg}$$

$$\dot{Q}_l = \frac{\dot{V}}{v} (W_o - W_i) * 2500$$

$$\dot{Q}_l = 3010 * \dot{V} * (W_o - W_i)$$

\dot{V} in l/s

39

Calculation of heat gains

Cooling Load due to Infiltration

ACH=Air Change per Hour=No of times the air changes in a building per hour

$$[l/s] = (ACH * V) * 1000 / 3600$$

V in m³

40

Calculation of heat gains

Cooling Load Due to Infiltration

$$ACH = a + bV + c(t_o - t_r)$$

Bldg. Construction	a	b	c
Tight	0.15	0.010	0.007
Average	0.20	0.015	0.014
Loose	0.25	0.020	0.022

T must be in deg C, and V must be in m/s

41

Calculation of heat gains

Cooling Load Due to Infiltration

$$\dot{V} [L/s] = ACH * V * 1000 / 3600$$

Sensible

$$\dot{Q}_s = 1.2 * \dot{V} * (t_o - t_r) \quad \text{Watts}$$

Latent

$$\dot{Q}_l = 3010 * \dot{V} * (W_o - W_r) \quad \text{Watts}$$

42

Cooling Load Due to Ventilation

Sensible $\dot{Q}_s = 1.2 * V * \rho * (t_o - t_r)$ **Watts**

Latent $\dot{Q}_l = 3010 * V * \rho * (W_o - W_r)$ **Watts**

V = Volume flow rate in L/s

43

Cooling Load Due to Partitions, Ceilings, & Floors

$$\dot{Q} = U A T D$$

TD=Temperature difference across the partition or floor

44

Example 12.5

Lights on at 7AM and off at 7PM

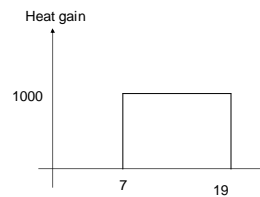
Heat due lights is 1000 W

Zone type =Medium, carpeted 50% glass

Lights: Un-vented suspended fluorescent lights

Radiative HG=0.67 HG

Convective HG=0.33 HG



45

Splitting Heat gain into convective and radiative portions

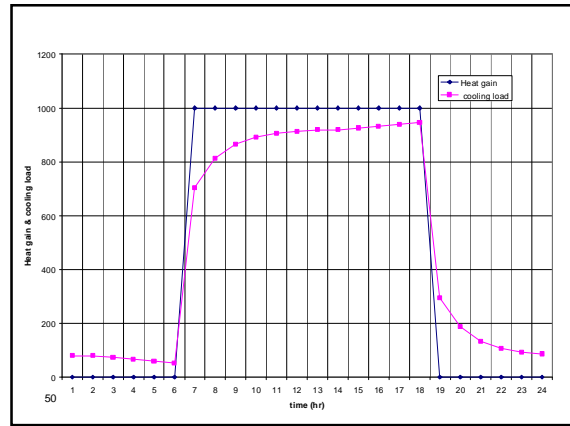
Heat Gain Source	Radiant Heat, %	Convective Heat, %
Transmitted solar, no inside shade	100	0
Window solar, with inside shade	63	37
Absorbed (by fenestration) solar	63	37
Fluorescent lights, suspended, unvented	67	33
recessed, vented to return air	59	41
recessed, vented to return air and supply air	19	81
Incandescent lights	80	20
Conduction, exterior walls	63	37
exterior roofs	84	16
Infiltration and ventilation	0	100
Machinery and appliances (see Table 13)	20 to 80	80 to 20

Source: Pedersen et al. (1998), Hsiao et al. (1999).

ts (hr)	Lights HG	Conv. HG [W] 0.33	Rad. HG [W] 0.67	RTS [Medium, Carpeted, 50 % glass]	Rad. CL [W]	Total CL [W]
1	0.0	0	0	0.49	80	80
2	0.0	0	0	0.17	80	80
3	0.0	0	0	0.09	74	74
4	0.0	0	0	0.05	67	67
5	0.0	0	0	0.03	60	60
6	0.0	0	0	0.02	54	54
7	1000	330	670	0.01	375	705
8	1000	330	670	0.01	482	812
9	1000	330	670	0.01	536	866
10	1000	330	670	0.01	563	893
11	1000	330	670	0.01	576	906
12	1000	330	670	0.01	583	913
13	1000	330	670	0.01	590	920
14	1000	330	670	0.01	590	920
15	1000	330	670	0.01	596	926
16	1000	330	670	0.01	603	933
17	1000	330	670	0.01	610	940
18	1000	330	670	0.01	616	946
19	0.0	0	0	0.01	295	295
20	0.0	0	0	0.01	188	188
21	0.0	0	0	0	134	134
22	0.0	0	0	0	107	107
23	0.0	0	0	0	84	84

ts (hr)	Lights HG	Conv. HG [W] 0.33	Rad. HG [W] 0.67	RTS [Medium, Carpeted, 50 % glass]	Rad. CL [W]	Total CL [W]
1	0.0	0	0	0.49	80	80
2	0.0	0	0	0.17	80	80
3	0.0	0	0	0.09	74	74
4	0.0	0	0	0.05	67	67
5	0.0	0	0	0.03	60	60
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20	0.0	0	0	0.01	188	188
21	0.0	0	0	0	134	134
22	0.0	0	0	0	107	107

ts (hr)	Lights HG	Conv. HG [W] 0.33	Rad. HG [W] 0.67	RTS [Medium, Carpeted, 50 % glass]	Rad. CL [W]	Total CL [W]
1	0.0	0	0	0.49	80	80
2	0.0	0	0	0.17	80	80
3	0.0	0	0	0.09	74	74
4	0.0	0	0	0.05	67	67
5	0.0	0	0	0.03	60	60
6	0.0	0	0	0.02	54	54
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19	0.0	0	0	0.01	295	295
20	0.0	0	0	0.01	188	188
21	49	0.0	0	0	134	134
22	0.0	0	0	0	107	107



Example 12.6 Solar heat gain and cooling load

The cooling load due a SSW window is to be calculated. The window is located in Jeddah, Saudi Arabia (July 21). 0.4% design outdoor conditions are assumed. Window is double one pane is bronze and the other is clear (type 5d). Window area is 10 m², U value is 3.24 W/m².K. The incidence angle, the beam radiation and the diffuse radiation are as given in the table below. Indoor and outdoor temperatures are also given.

51

Time (hr)	t_o	t_i	θ	C_{b1} [W/m ²]	G_b [W/m ²]
1	29.6	25	>90	0	0
2	29.0	25	>90	0	0
3	28.5	25	>90	0	0
4	28.1	25	>90	0	0
5	28.0	25	131.2	0	0
6	28.2	25	124.3	0	22
7	28.9	25	116.8	0	81.5
8	30.0	25	109.1	0	125
9	31.5	25	101.7	0	158.8
10	33.4	25	95.0	0	183.7
11	35.4	25	88.9	0	206
12	37.4	25	84.2	14.5	217.3
13	38.9	25	81	89.1	216.7
14	39.8	25	79.6	134.1	204
15	40.2	25	80.2	147.7	179.9
16	39.8	25	82.6	128.2	143.8
17	39.0	25	>90	78.2	94.8
18	37.6	25	>90	12.8	35.8
19	35.1	25	>90	0	0
20	34.5	25	>90	0	0
21	33.1	25	>90	0	0
22	31.9	25	>90	0	0
23	30.9	25	>90	0	0

Time (hr)	t_o	t_i	C_{b1} [W/m ²]	SHGC ₀	Direct HG	RTS Solar	Cooling load (Direct Solar)	G_t [W/m ²]	SHGC _d
1	29.6	25	0	0	0	0.54	9	0	0.414
2	29.0	25	0	0	0	0.16	9	0	0.414
3	28.5	25	0	0	0	0.08	9	0	0.414
4	28.1	25	0	0	0	0.04	9	0	0.414
5	28.0	25	0	0	0	0.03	9	0	0.414
6	28.2	25	0	0	0	0.02	9	22	0.414
7	28.9	25	0	0	0	0.02	8	81.5	0.414
8	30.0	25	0	0	0	0.01	6	125	0.414
9	31.5	25	0	0	0	0.01	3	158.8	0.414
10	33.4	25	0	0	0	0.01	1	183.7	0.414
11	35.4	25	0	0	0	0.01	0	206	0.414
12	37.4	25	14.5	0.05	7	0.01	4	217.3	0.414
13	38.9	25	89.1	0.11	58	0.01	54	216.7	0.414
14	39.8	25	134.1	0.16	215	0.01	130	204	0.414
15	40.2	25	147.7	0.17	251	0.01	178	179.9	0.414
16	39.8	25	128.2	0.17	218	0.01	170	143.8	0.414
17	39.0	25	78.2	0.13	102	0.01	122	94.8	0.414
18	37.6	25	12.8	0.09	12	0.01	58	35.8	0.414
19	35.1	25	0	0	0	0	32	0	0.414
20	34.5	25	0	0	0	0	20	0	0.414
21	33.1	25	0	0	0	0	14	0	0.414
22	31.9	25	0	0	0	0	10	0	0.414
23	30.9	25	0	0	0	0	0	0	0.414

hr	t_o	t_i	G_t [W/m ²]	SHGC _d	Dir. HG	Conductive	Cond-DBI	Conv (0.37)	Rad (0.83)	CL Rad (cond-DBI)	CL Conv-DBI	Total Cooling load
1	29.6	25	0	0.414	0	140	140	55	94	171	226	236
2	29.0	25	0	0.414	0	129	129	48	81	160	207	218
3	28.5	25	0	0.414	0	113	113	42	71	146	190	199
4	28.1	25	0	0.414	0	101	101	37	64	137	175	184
5	28.0	25	0	0.414	0	97	97	36	61	128	164	173
6	28.2	25	22	0.414	81	105	106	73	124	151	223	232
7	28.9	25	81.5	0.414	337	120	402	171	291	236	407	415
8	30.0	25	125	0.414	578	140	678	251	407	326	579	585
9	31.5	25	158.8	0.414	857	212	889	322	546	407	742	748
10	33.4	25	183.7	0.414	781	271	1052	382	595	595	886	890
11	35.4	25	206	0.414	853	338	1191	441	750	580	1030	1030
12	37.4	25	217.3	0.414	950	402	1301	481	830	688	1139	1143
13	38.9	25	216.7	0.414	837	440	1346	498	848	703	1202	1206
14	39.8	25	204	0.414	846	481	1325	490	835	721	1211	1243
15	40.2	25	179.9	0.414	746	482	1237	458	779	707	1165	1243
16	39.8	25	143.8	0.414	536	481	1076	398	678	688	1056	1205
17	39.0	25	94.8	0.414	332	453	845	313	533	573	886	1007
18	37.6	25	35.8	0.414	107	409	516	191	325	442	633	692
19	35.1	25	0	0.414	0	358	358	132	226	346	478	510
20	34.5	25	0	0.414	0	307	307	113	193	290	403	423
21	33.1	25	0	0.414	0	251	251	97	166	251	340	362
22	31.9	25	0	0.414	0	224	224	83	141	223	305	316
23	30.9	25	0	0.414	0	192	192	71	121	201	272	281
24	30.2	25	0	0.414	0	160	160	62	106	164	240	258

Heat Gain Source	Radiant Heat, %	Convective Heat, %
Transmitted solar, no inside shade	100	0
Window solar, with inside shade	63	37
Absorbed (by fenestration) solar	63	37
Fluorescent lights, suspended, unvented	67	33
recessed, vented to return air	59	41
recessed, vented to return air and supply air	19	81
Incandescent lights	80	20
Conduction, exterior walls	63	37
exterior roofs	84	16
Infiltration and ventilation	0	100
Machinery and appliances (see Table 3.3)	20 to 80	80 to 20

Sources: Pefferman et al. (1996), Hens et al. (1999).

55

Heat Gain Type	Recommended Radiative Fraction	Recommended Convective Fraction
Occupants (60)	0.7	0.3
Lighting (60%)		
Fluorescent fluorescent—		
suspended	0.67	0.33
recessed	0.59	0.41
vented to return air	0.19	0.81
vented to supply and		
return air		
incandescent	0.80	0.20
Equipment		
General office/electronic	0.7	0.3
equipment not internally		
cooled (e.g. fans)		
Computer/electronic	0.2	0.8
equipment with internal		
fans		
Conduction heat gain		
through walls (1)	0.63	0.37
Conduction heat gain		
through roofs (1)	0.84	0.16
Through (roof) walls	0.6	0.0
conduction		
Absorbed solar radiation	0.63	0.37
Infiltration	0.0	1.0

56