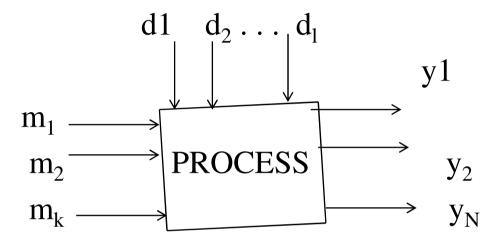
Modeling Difficulties

- Poorly Known Processes
 - V-L and L- L thermodynamic equlb. In multi-component distillation
 - Multi-component reaction systems
 - Interaction between heat, mass and momentum
- Error in model parameters
 - U (over all heat transfer coefficient)
 - T_d
 - K_o and E in $k=k_o$ $e^{E/RT}$
- Complexity of model (
 Distillation column with N trays need [2N+4] equations

Accurate model — Complex

Input-Output Model

Convenient for control purposes



$$y_i = f(m_1, m_2, ..., m_k, d_1, d_2,...,d_l)$$

$$i = 1,2,3,...,n$$

Solution of ODEs

- Modeling results in nonlinear sets of ordinary differential equations
- Solution requires numerical integration
- To get solution, we must first:
 - specify all constants (densities, heat capacities, etc, ...)
 - specify all initial conditions
 - specify types of perturbations of the input variables

For the heated stirred tank,

$$\frac{dT}{dt} = \frac{F}{V}(T_{in} - T) + \frac{Q}{\rho V C_P}$$

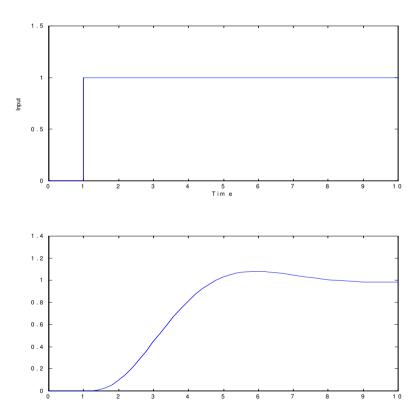
- specify ρ , C_{P_1} and V
- specify T(0)
- specify Q(t) and F(t)

Input Specifications

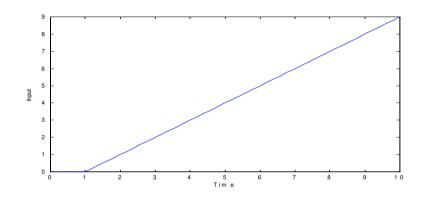
- Study of control system dynamics
 Observe the time response of a process output to input changes
- Focus on specific inputs
 - 1. Step input signals
 - 2. Ramp input signals
 - 3. Pulse and impulse signals
 - 4. Sinusoidal signals
 - 5. Random (noisy) signals

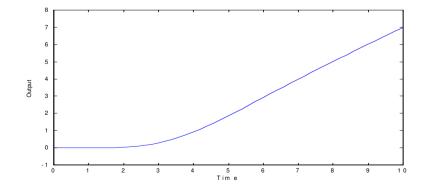
1. Step Input Signal: a sustained instantaneous change

e.g. Unit step input introduced at time 1



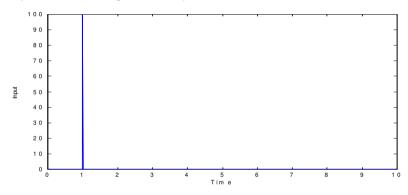
2. Ramp Input: A sustained constant rate of change e.g.

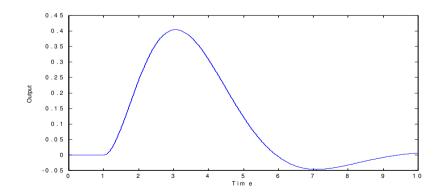




3. Pulse: An instantaneous temporary change

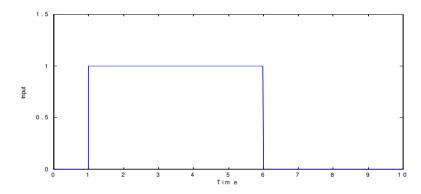
e.g. Fast pulse (unit impulse)

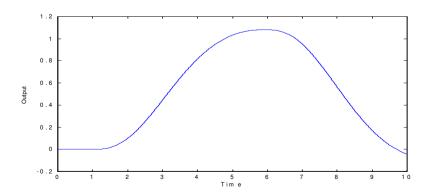




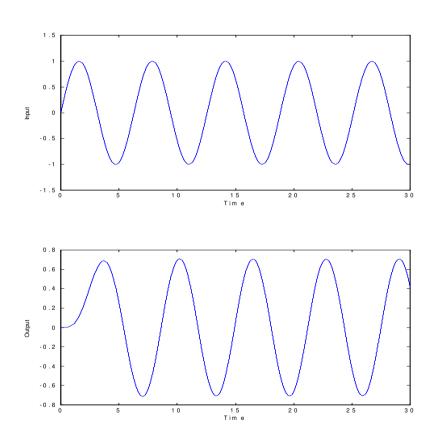
3. Pulses:

e.g. Rectangular Pulse





4. Sinusoidal input



Laplace Transform

$$F(s) = L(f(t)) = \int_{0}^{\infty} f(t)e^{-st} dt$$

f(t) has to be at least stepwise continues

It is transform. from time domain (t) to Laplace domain (s)

$$S = a+bj$$

Common Transforms

1. Constant

$$f(t) = a$$

$$\Im[a] = \int_{0}^{\infty} ae^{-st} dt = (-ae^{-st}/s)_{0}^{\infty} = a/s$$

2. Step

$$f(t) = \begin{cases} 0 & t < 0 \\ a & t \ge 0 \end{cases}$$

$$\Im[f(t)] = \int_{0}^{\infty} ae^{-st} dt = (-ae^{-st}/s)_{0}^{\infty} = a/s$$

3. Ramp function

$$f(t) = \begin{cases} 0 & t < 0 \\ at & t \ge 0 \end{cases}$$

$$\Im[f(t)] = \int_{0}^{\infty} ate^{-st} dt = -\frac{e^{-st}at}{s} \bigg]_{0}^{\infty} + \int_{0}^{\infty} \frac{ae^{-st}}{s} dt = \frac{a}{s^{2}}$$

4. Rectangular Pulse

$$f(t) = \begin{cases} 0 & t < 0 \\ a & 0 \le t < t_w \\ 0 & t \ge t_w \end{cases}$$
$$\Im[f(t)] = \int_{0}^{t_w} ae^{-st} dt = \frac{a}{s} (1 - e^{-t_w s})$$

5. Unit impulse

$$\Im[\mathcal{S}(t)] = \lim_{t_w \to 0} \frac{1}{t_w s} (1 - e^{-t_w s})$$

$$\Im[\mathcal{S}(t)] = \lim_{t_w \to 0} \frac{se^{-t_w s}}{s} = 1$$

1. Exponential

$$f(t) = e^{-bt}$$

$$\Im[e^{-bt}] = \int_0^\infty e^{-bt} e^{-st} dt = \int_0^\infty e^{-(s+b)t} dt$$

$$\Im[e^{-bt}] = -\frac{e^{-(s+b)t}}{s+b} \Big]_0^\infty = \frac{1}{s+b}$$

2. Cosine

$$f(t) = \cos(\omega t) = \frac{e^{-j\omega t} + e^{j\omega t}}{2}$$

$$\Im[\cos(\omega t)] = \frac{1}{2} \left\{ \int_{0}^{\infty} e^{-(s-j\omega)t} dt + \int_{0}^{\infty} e^{-(s+j\omega)t} dt \right\}$$
$$= \frac{1}{2} \left\{ \frac{1}{s-j\omega} + \frac{1}{s+j\omega} \right\} = \frac{s}{s^2 + \omega^2}$$

Common Transforms

3. Sine (ωt)

$$f(t) = \sin(\omega t) = \frac{e^{j\omega t} - e^{-j\omega t}}{2j}$$

$$\Im[\sin(\omega t)] = \frac{1}{2j} \left\{ \int_{0}^{\infty} e^{-(s-j\omega)t} dt - \int_{0}^{\infty} e^{-(s+j\omega)t} dt \right\}$$

$$= \frac{1}{2j} \left\{ \frac{1}{s - j\omega} - \frac{1}{s + j\omega} \right\} = \frac{\omega}{s^2 + \omega^2}$$

Common Transforms

1. Derivative of a function f(t)

$$\frac{df(t)}{dt}$$

$$du = df$$

$$v = e^{-st}$$

$$\Im\left[\frac{df}{dt}\right] = uv\right]_0^{\infty} - \int_0^{\infty} u dv = f(t)e^{-st}\Big]_0^{\infty} - \int_0^{\infty} (-sf(t)e^{-st}) dt$$

$$\Im\left[\frac{df}{dt}\right] = s\int_0^{\infty} f(t)e^{-st} dt - f(0) = sF(s) - f(0)$$

2. Integral of a function f(t)

$$\Im\begin{bmatrix} t \\ \int f(\tau)d\tau \end{bmatrix} = \int_{0}^{\infty} e^{-st} (\int_{0}^{t} f(\tau)d\tau)dt = \frac{F(s)}{s}$$

Laplace Transforms

Final Value Theorem

$$\lim_{t \to \infty} [y(t)] = \lim_{s \to 0} [sY(s)]$$

Initial Value Theorem

$$y(0) = \lim_{s \to \infty} [sY(s)]$$

Algorithm for Solution of ODEs

- Take Laplace Transform of both sides of ODE and boundary conditions.
- Solve for Y(s)=p(s)/q(s)
- Factor the characteristic polynomial q(s)
- Perform partial fraction expansion
- Inverse Laplace using Tables of Laplace Transforms

Partial fraction Expansions

1. q(s) has real and distinct roots

$$q(s) = \prod_{i=1}^{n} (s + b_i)$$

expand as

$$r(s) = \sum_{i=1}^{n} \frac{\alpha_i}{s + b_i}$$

2. q(s) has real but repeated roots

$$q(s) = (s+b)^n$$

expanded

$$r(s) = \frac{\alpha_1}{s+b} + \frac{\alpha_2}{(s+b)^2} + \frac{\alpha_n}{(s+b)^n}$$

q(s) has imajnary rootsroots comes in the form of complex conjugates:

$$r_1, r_2 = a \pm b i$$

a = real part

b = imaginary part

$$r(s) = \frac{\alpha 1}{s + a i} + \frac{\alpha 1}{s - bi}$$

General solution:

$$Y(t) = C_1 e^{-p1t} + C_2 e^{-p2t} + \dots + C_n e^{-pnt} + C_{11} e^{-p11t} + C_{12} t e^{-p12t} + \dots$$

$$C_{1m} t_{m-1} e^{-pm-1t} + C_{21} e^{-at} + C_{21}^* e^{bjt}$$

Example 8.1

$$a_2 d^2y/dt^2 + a_1 dy/dt + a_0y(t) = f(t)$$
 $f(t)$ is a unit step $(f(t)=1)$
 $y(o) = y`(o) = 0$
 $cas 1: a_1=4, a_2=1, a_0=3$
 $r_1=0, r_2=r_3=-1$
 $cas 2: a_1=2, a_2=1, a_0=1$
 $r_1=0, r_2=-1, r_3=-3$
 $cas 3: a_1=2, a_2=2, a_0=1$
 $r_1=0, r_2=-1, r_3=-3$

Transfer Functions

A linear, n^{th} -order system is:

$$a_n \frac{d^n y}{dt^n} + a_{n-1} \frac{d^{n-1} y}{dt^{n-1}} + a_1 \frac{d y}{dt} + a_0 y = b f(t)$$

With initial conditions: $y(0) = y^(0) = y^(0) = \dots y^{(n-1)}(0) = 0$

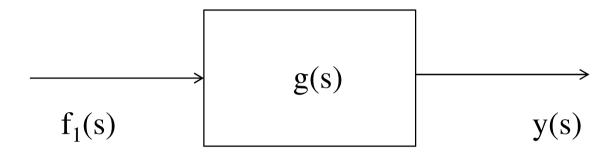
$$a_n s^n y(s) + a_{n-1} s^{n-1} y(s) + s^{n-2} y(s) + a_1 s y(s) + a_0 y(s) = b f(s)$$

$$y(s)(a_ns^n+a_{n-1}s^{n-1}+s^{n-2}....+a_1s+a_0) = b f(s)$$

$$\frac{y(s)}{f(s)} = \frac{b}{(a_n s^n + a_{n-1} s^{n-1} + ... + a_1 s + a_0)} = g(s) = \underbrace{Output}_{Input}$$

g(s) is the transfer function

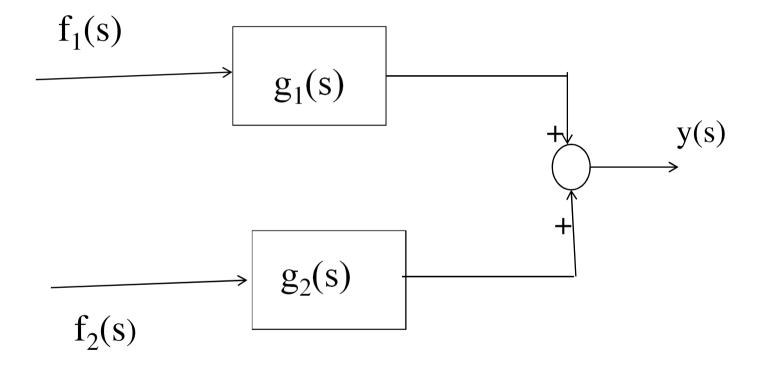
$$y(s) = g(s) *f(s)$$



For two inputs f_1 and f_2 :

$$y(s) = \frac{b_1 f_1(s)}{(a_n s^n + a_{n-1} s^{n-1} + \dots + a_1 s + a_0)} + \frac{b_2 f_2(s)}{(a_n s^n + a_{n-1} s^{n-1} + \dots + a_1 s + a_0)}$$

$$y(s) = g_1(s) * f_1(s) + g_2(s) * f_2(s)$$



Note that the denominator of $g_1(s)$ and $g_2(s)$ are the same. It is called characteristic equation.

Poles and zeros of Trasfer Function

$$g(s) = \frac{Q(s)}{P(s)}$$

 $P(s) \equiv$ Characteristic Polynomial

Q(s) has a lower order than P(s)

Roots of Q(s) are called zeros of T. F. (g(s) = 0 at zeros)

Roots of P(s) are called poles of T. F. $(g(s) = \infty \text{ at poles})$

They play important roles in dynamics

$$\frac{y(s)}{f(s)} = g(s) \longrightarrow y(s) = g(s)*f(s)$$

If f(t) is given take L. T. of $f(t) \longrightarrow y(t) = L^{-1} [g(s) * f(s)]$

$$g(s) = \frac{Q(s)}{P(s)} = \frac{Q(s)}{(s-p_1)(s-p_2)(s-p_3)^m(s-p_4)(s-p_4^*)}$$

wher p_1 , p_2 , p_3 , p_4 , p_4^* are roots of P(s)

$$g(s) = \frac{Q(s)}{P(s)} = \frac{C_1}{(s-p_1)} + \frac{C_2}{(s-p_2)} + \frac{C_{31}}{(s-p_3)} + \frac{C_{32}}{(s-p_3)^2} + \dots + \frac{C_{3m}}{(s-p_3)^m} + \frac{C_4}{(s-p_4)} + \frac{C_{*4}}{(s-p_4)}$$

$$f(t) = C \longrightarrow f(s) = C/s$$

$$y(t) = L^{-1} [g(s) * f(s)] = L^{-1} [g(s) * C/s]$$

$$y(t) = C_0 + C_1 e^{p1t} + C_2 e^{p2t} + [C_{31} + C_{32} t + C_{33} t^2 + + C_{3m} t^{m-1}] e^{p3t} + C_4 e^{p4t}$$

$$1! \qquad 2! \qquad (m-1)!$$

 $+C_{4}^{*}C^{p*4t}$

$$p_4 = a + bj$$

$$p^*_{4} = a - bj$$

$$e^{p4t} = e^{(a+bj)t} = e^{at} \cdot e^{bjt} = e^{at} [\cos(bt) + j \sin(bt)]$$

$$e^{p*4t} = e^{(a-bj)t} = e^{at} \cdot e^{-bjt} = e^{at} [\cos(bt) - j \sin(bt)]$$

y(t) is stable if all poles and the real parts of the complex conjugates are

negatives
$$(p_i \text{ and } a_i < 0) \longrightarrow y(t) = C_0 \text{ as } t \rightarrow \infty$$

y(t) is unstable if any of p_i and a_i are $> 0 \longrightarrow y(t) \rightarrow \infty$ as $t \rightarrow \infty$

y(t) is marginally stable of all p_i and $a_i = 0$

First-order systems

Time-domain model First order process

Laplace-domain model

$$a_1 \frac{\mathrm{d} y}{\mathrm{d} t} + a_0 y = b u(t)$$

 $(a_0 \neq 0, dividing by a_0)$

$$\tau_P \frac{\mathrm{d} y}{\mathrm{d} t} + y = K_P u(t)$$

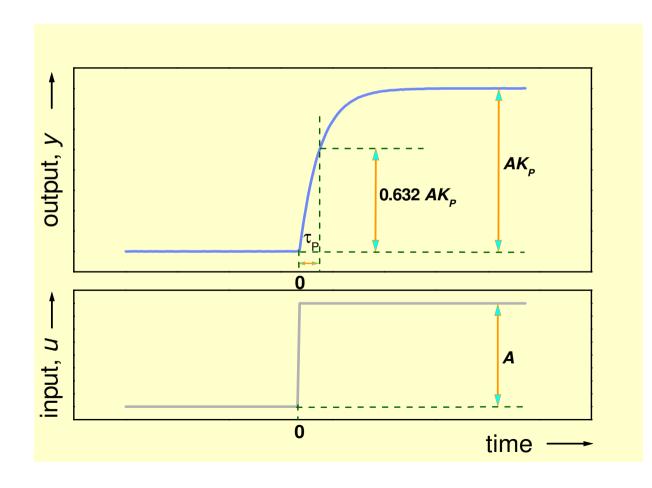
$$y(s) = \left(\frac{K_P}{\tau_P s + 1}\right) u(s)$$

- K_P (b/a₀ is the process *steady state gain* (it can be >0 or <0)
- \bullet τ_P (a₁/a₀) is the process *time constant* (it is always >0)
- Transfer function of a first-order system:

$$G(s) = \frac{K_P}{\tau_P s + 1}$$

Response of first-order systems

• We only consider the response to a step forcing function of amplitude A



The time-domain response is:

$$y(t) = AK_P \left(1 - e^{-\frac{t}{\tau_P}} \right)$$

Determining the process gain

An open-loop test can be performed starting from the reference steady state:

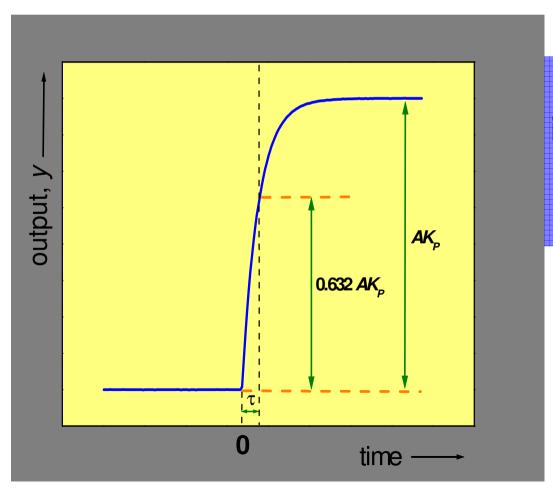
- step the input to the process
- record the time profile of the measured output until a new steady state is approached
- check if this profile resembles $y(t) = AK_P(1 e^{-t/\tau_P})$
- if so, calculate K_P as:

$$K_{P} = \frac{y_{ss,new} - y_{ss,ref}}{u_{new} - u_{ref}} = \left(\frac{\Delta(\text{output})}{\Delta(\text{input})}\right)_{steady state}$$

The process gain can be determined from steady state information only

Determining the time constant

- From the same open-loop test:
 - determine τ_P graphically (note: it has the dimension of time)



You need <u>dynamic</u>
information to determine
the process time
constant

Determining the values of K_P and τ_P from process data is known as *process identification*

Pure capacity process

$$a_1 \frac{\mathrm{d} y}{\mathrm{d} t} + a_0 y = b f(t)$$

Let $a_0 = 0$ then

$$a_1 \frac{\mathrm{d} y}{\mathrm{d} t} = b f(t)$$
 divide by $a_1 \text{ gives } \frac{\mathrm{d} y}{\mathrm{d} t} = (b/a_1) f(t)$

$$\frac{\mathrm{d} y}{\mathrm{d} t} = K \hat{f}(t) \quad \text{take L. T.}$$

$$y(s) = K^s$$

Pure capacity process

Second-order systems

■ Time-domain representation:

$$a_2 \frac{d^2 y}{dt^2} + a_1 \frac{d y}{dt} + a_0 y = bu(t)$$

Dividing by a_0 where $a_0 \neq 0$

$$(a_2/a_0)\frac{d^2y}{dt^2} + (a_1/a_0)\frac{dy}{dt} + y = (b/a_0)u(t)$$

$$\tau^2 \frac{\mathrm{d}^2 y}{\mathrm{d}t^2} + 2\zeta \tau \frac{\mathrm{d}y}{\mathrm{d}t} + y = K_p u(t)$$

 K_p = process gain τ = natural period ζ = damping coefficient Laplace-domain representation: •

$$\frac{Y(s)}{U(s)} = \frac{K_p}{\tau^2 s^2 + 2\zeta \tau s + 1}$$

Three cases of processes:

Overdamped $\xi 1$

Critically Damped $\xi = 1$

Underdamped ξ <1

Note: Chemical processes are typically overdamped or critically damped

Second Order Processes

Roots of the characteristic polynomial

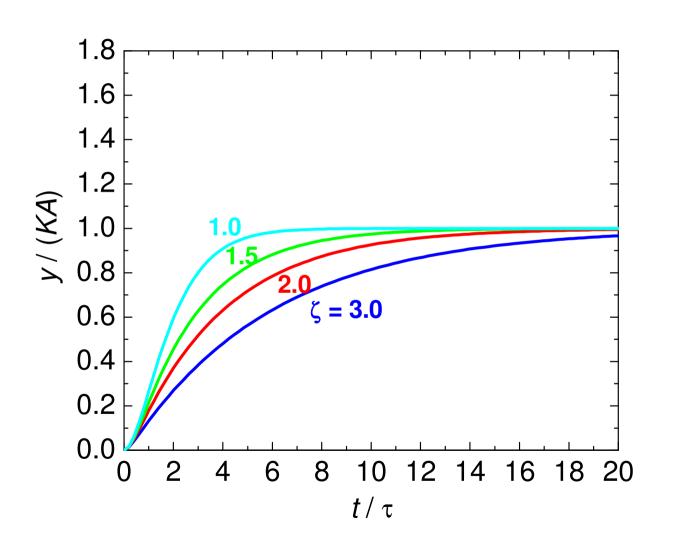
$$\frac{-2\xi\tau \pm \sqrt{4\xi^{2}\tau^{2} - 4\tau^{2}}}{2\tau^{2}} \\ -\frac{\xi}{\tau} \pm \frac{1}{\tau} \sqrt{\xi^{2} - 1}$$

Case 1) ξ >1: Two distinct real roots System has an exponential behavior

Case 2) ξ =1: One multiple real root Exponential behavior

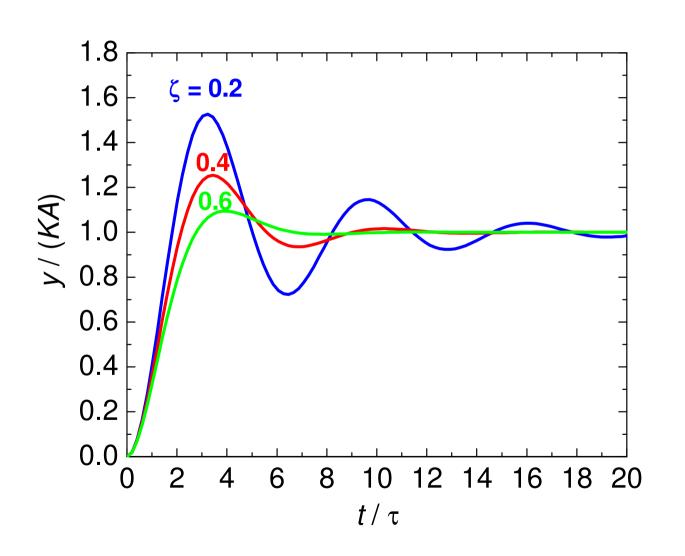
Case 3) ξ <1: Two complex roots System has an oscillatory behavior

Overdamped systems (ξ >1)



Open-loop response to a input step disturbance

Underdamped systems (ξ <1)

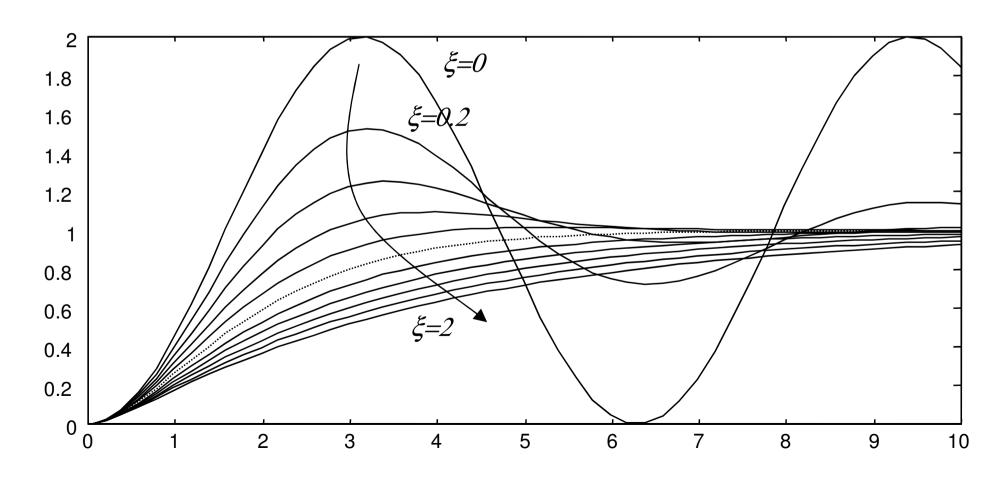


Open-loop response to a input step disturbance

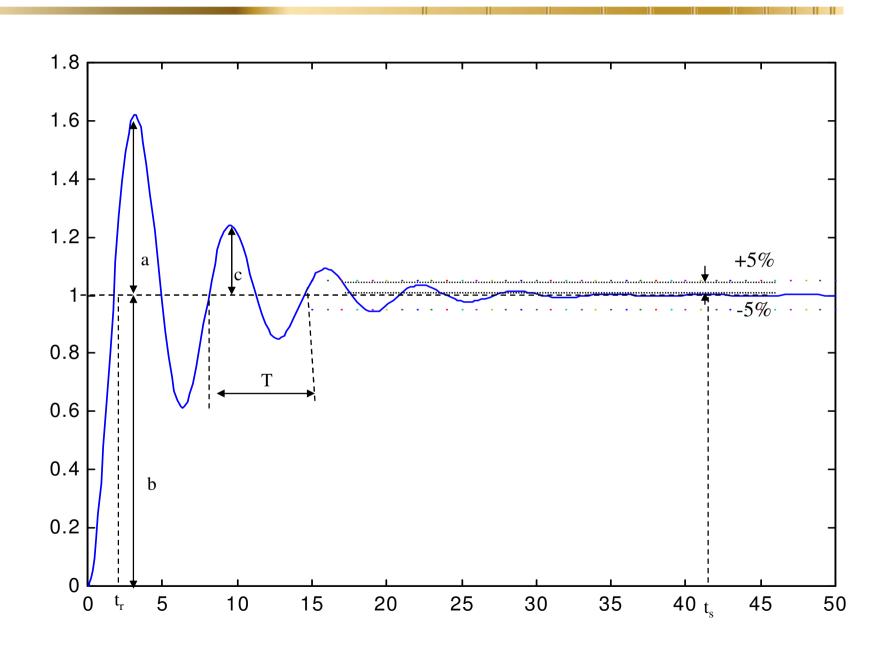
Second order Processes

Step response of magnitude M

$$Y(S) = \frac{K_{P}}{\tau^{2} s^{2} + 2\xi \tau s + 1} \frac{M}{s}$$



Characteristics of underdamped second order process



Characteristics of underdamped second order process

- 1. Rise time, t_r
- 2. Settling time (response time), t_s
- 3. Overshoot:

$$OS = \frac{a}{b} = \exp\left(-\frac{\xi}{\sqrt{1-\xi^2}}\pi\right)$$

5. Decay ratio:

$$DR = \frac{c}{b} = \exp\left(-\frac{2\pi\xi}{\sqrt{1-\xi^2}}\right)$$

Period of oscillation (T)

$$T = 2\pi \tau / (1-\xi^2)^{1/2}$$
 $\omega = radian frequency = (1-\xi^2)^{1/2} / \tau$